

AD-A092 568

NAVAL RESEARCH LAB WASHINGTON DC

F/G 4/1

SCALE SIZES AND LIFETIMES OF F REGION PLASMA CLOUD STRIATIONS A--ETC(U)

NOV 80 B E MCDONALD, S L OSSAKOW, S T ZALESAK

UNCLASSIFIED

NRL-MR-4383

NL

For 1  
ALL 5  
0-20 PUGH



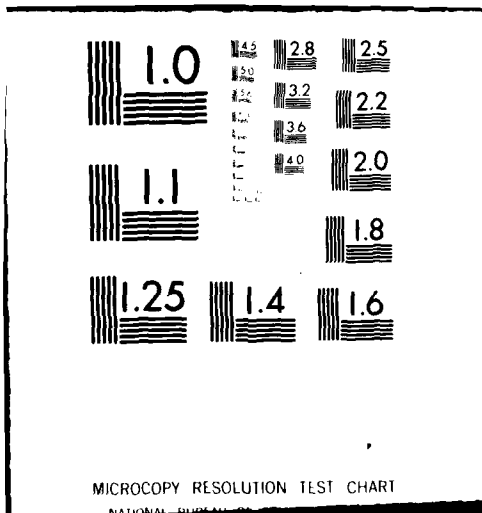
END

DATE

FILED

1-81

DTIC



AD A092568

⑨ Memorandum rept.

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

| REPORT DOCUMENTATION PAGE   |                                  | READ INSTRUCTIONS<br>BEFORE COMPLETING FORM                                    |  |
|---|----------------------------------|--|--|
| 1. REPORT NUMBER<br>NRL Memorandum Report 4383  | 2. GOVT ACCESSION NO.<br>AD-A092 | 3. RECIPIENT'S CATALOG NUMBER<br>568   |  |
| 4. TITLE (and Subtitle)<br>SCALE SIZES AND LIFETIMES OF F REGION PLASMA<br>CLOUD STRIATIONS AS DETERMINED BY THE<br>CONDITION OF MARGINAL STABILITY.  |                                  | 5. TYPE OF REPORT & PERIOD COVERED<br>Interim report on a continuing<br>basis. |  |
| 7. AUTHOR(s)<br>B. E. McDonald, S. L. Ossakow, S. T. Zalesak, and<br>N. J. Zabusky  |                                  | 8. CONTRACT OR GRANT NUMBER(s)<br>11 17 Nov 80                                 |  |
| 9. PERFORMING ORGANIZATION NAME AND ADDRESS<br>Naval Research Laboratory<br>Washington, DC 20375  |                                  | 10. PROGRAM ELEMENT, PROJECT, TASK<br>AREA & WORK UNIT NUMBERS<br>67-0889-0-0  |  |
| 11. CONTROLLING OFFICE NAME AND ADDRESS<br>Defense Nuclear Agency<br>Washington, DC 20305   |                                  | 12. REPORT DATE<br>November 17, 1980   |  |
| 14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)   |                                  | 13. NUMBER OF PAGES<br>41  |  |
|   |                                  | 15. SECURITY CLASS. (of this report)<br>UNCLASSIFIED                           |  |
|   |                                  | 15a. DECLASSIFICATION/DOWNGRADING<br>SCHEDULE                                  |  |
| 16. DISTRIBUTION STATEMENT (of this Report)<br><br>Approved for public release: distribution unlimited.   |                                  |  |  |
| 17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)<br><br>DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)  |                                  |  |  |
| 18. SUPPLEMENTARY NOTES<br>*Present address: University of Pittsburgh, Pittsburg, PA<br>This research was sponsored by the Defense Nuclear Agency under subtask S99QAXHC041,<br>work unit 21, and work unit title "Plasma Structure Evolution."   |                                  |  |  |
| 19. KEY WORDS (Continue on reverse side if necessary and identify by block number)<br>Plasma striations      Computer simulations<br>Gradient drift<br>Bifurcation<br>Striation "freezing"<br>Scale sizes   |                                  |  |  |
| 20. ABSTRACT (Continue on reverse side if necessary and identify by block number)<br>The two dimensional integrated Pedersen conductivity model for F region plasma cloud<br>striation development may be cast in dimensionless form. The result implies that a structure's<br>stability against bifurcation depends upon whether a diffusion parameter R exceeds a critical<br>value. The critical R for striations is determined by high resolution computer simulation for con-<br>ductivity ratios M from 2 to 30. Our results combined with electron diffusivity of order 1 m <sup>2</sup> /sec<br>agree with observed minimum scale sizes of 15 meters. For turbulent diffusivity of order<br><br>(Continues) |                                  |  |  |

DD FORM 1 JAN 73 1473

EDITION OF 1 NOV 65 IS OBSOLETE  
S/N 0102-LF-014-6601

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

254950

20. Abstract (continued)

→ 100  $\text{m}^2/\text{sec}$ , our results agree with frequent observations of kilometer-scale structures which "freeze up" and last for times of order  $10^4$  seconds. This lifetime is also predicted by our results.

# CONTENTS

|  |    |
|--|----|
| 1. INTRODUCTION .....                              | 1  |
| 2. EQUATIONS OF MOTION FOR THE ONE LEVEL MODEL ... | 3  |
| 3. NUMERICAL SIMULATIONS .....                     | 7  |
| 4. RESULTS .....                                   | 11 |
| 5. SUMMARY AND COMPARISON WITH DATA .....          | 23 |
| ACKNOWLEDGMENT .....                               | 27 |
| REFERENCES .....                                   | 28 |

|                     |                                     |
|---------------------|-------------------------------------|
| Accession For       |                                     |
| NTIS GRA&I          | <input checked="" type="checkbox"/> |
| DTIC TAB            | <input type="checkbox"/>            |
| Unannounced         | <input type="checkbox"/>            |
| Justification       |                                     |
| By _____            |                                     |
| Distribution/ _____ |                                     |
| Availability Codes  |                                     |
| Dist                | Avail and/or<br>Special             |
| <b>A</b>            |                                     |

# SCALE SIZES AND LIFETIMES OF F REGION PLASMA CLOUD STRIATIONS AS DETERMINED BY THE CONDITION OF MARGINAL STABILITY

## 1. Introduction

Phenomenologists have been pressed to account for certain features of late time barium cloud striations, despite the early time success and near universal acceptance of results from the  $E \times B$  gradient drift instability theory [Linson and Workman, 1970; Perkins et al., 1973, Francis and Perkins, 1975].

We refer to the simultaneous occurrence of three phenomena as documented in the 1977 STRESS program: a) the generation of structure on scales as small as 15 meters [Baker and Ulwick, 1978]; b) the apparent ubiquity of visible striations separated by distances approaching one kilometer; and c) the survival for hours (sometimes referred to as "freezing up") of this kilometer-scale structure as evidenced by propagation studies [Prettie et al., 1977]. If the gradient drift instability is at work producing small structure through a series of bifurcations, why do the kilometer scale structures persist? What parameters select out the kilometer scale size so often?

(Observers have often noted that visible structuring seems to halt when scale sizes transverse to the neutral wind direction decrease to just under one kilometer [J. A. Fedder, W. Chestnut, private communication, 1980]. Past this point, there is a tendency for the striations to drift in unison as long as they can be seen.)

We support the gradient drift instability as the explanation for striation behavior. In fact, the emergence at late times of density power law spectra from numerical simulations [Scannapieco, et al. 1976] is in agreement with observation [Baker and Ulwick, 1978]. We feel, however, that attempts to explain the above mentioned three features have been hindered by approaching the problem from two opposite extremes: 1) application of analytic

Manuscript submitted September 29, 1980.

results from an idealized one dimensional slab model; and 2) brute force case-by-case numerical simulation beginning with an initially smooth plasma distribution, and proceeding toward a highly structured state. One is not surprised that some disagreement exists between an idealized linear result and the highly structured nonlinear environment. On the other extreme, global numerical simulation on present day computers must eventually be hindered by inadequate resolution. We feel, too, that the role of diffusion (both classical and turbulent) has not been sufficiently emphasized in determining late time structure. This is partly because present day computers cannot resolve both the global cloud scale and the diffusion scale due to storage and speed limitations. In order to fill in these gaps, we shall extract from the basic one level (F region) striation model a scaling law which allows individual structures to provide information concerning "bifurcation tendencies" applicable to other similar structures of arbitrary size. We demonstrate in Section 2 that bifurcation or non-bifurcation of a particular structure hinges upon whether a diffusion parameter  $R$ , analogous to the Reynolds number for neutral flows, exceeds a critical value. This  $R$  value provides an estimate for the scale size of the state of marginal bifurcation tendency. It also provides an estimate for the lifetime of the marginal state. We determine the critical  $R$  by high resolution numerical simulation of an isolated structure of relevant geometry. Just enough physical diffusion is added to prevent bifurcation and loss of resolution.

We are aware that mechanisms other than diffusion can affect structure on suitable scales. Among these are inertial forces, kinetic (finite gyroradius) effects, and E-to-F layer coupling. It is our desire, however, to present the most basic model which seems to agree with the stated observations. In order to explain the side-by-side existence at late times of



15 meter and kilometer scale sizes [Baker and Ulwick, 1978] we hypothesize that the cloud is dominated by turbulent diffusivity of order  $100 \text{ m}^2/\text{sec}$ , but that selected regions may reflect non turbulent electron diffusion of order  $1 \text{ m}^2/\text{sec}$ .

In Section 3 we describe the numerical techniques by which the equations of motion are solved. These techniques reflect appropriate advances in the state-of-the-art since the early simulations of large scale striation morphology [Zabusky, et al., 1973; Scannapieco, et al., 1974, 1976]. The scaling derived in Section 2 allows us to simulate a small region of the plasma with adequate resolution, providing that boundary conditions can be specified appropriately. Section 4 contains results of the numerical simulations and illustrates how the critical R depends upon the conductivity ratio M. In Section 5 we show that our calculated R values are compatible with rocket probe data on scales of tens of meters [Baker and Ulwick, 1978]. We show that if turbulent diffusivity is operative, a wide range of conditions will lead to marginally stable scale sizes of approximately one kilometer. In addition, we predict that the lifetime of the kilometer-scale structure should be of order  $10^4$  sec., in agreement with propagation experiments conducted during the STRESS program [Prettie et al., 1977]. Thus it is possible that our results may help to explain the "freezing up" of visible kilometer-scale barium cloud structures [J. A. Fedder, W. Chestnut, private communication, 1980].

## 2. Equations of Motion for the One Level Model

The two dimensional field line integrated Pedersen conductivity model appropriate to F-region clouds consists of the following equations (in cgs units) which are cast in a frame drifting with the ambient plasma:

$$\frac{\partial \Sigma}{\partial t} = - \nabla \cdot \Sigma \underline{v} + K \nabla^2 \Sigma \quad (1)$$

$$\underline{V} = - \frac{c}{B} \nabla \phi \times \underline{\hat{z}} \quad (2)$$

$$\nabla \cdot \Sigma \nabla \phi = E_o \frac{\partial \Sigma}{\partial y}, \quad (3)$$

where  $\Sigma$  is the magnetic field-line-integrated Pedersen conductivity,  $K$  is the cross-field diffusivity of the cloud plasma,  $\underline{V}$  is the local plasma drift relative to the ambient drift velocity,  $c$  is the speed of light,  $B = B \underline{\hat{z}}$  is the constant magnetic field strength,  $\phi$  is the induced electrostatic potential, and  $\underline{E}_o = E_o \underline{\hat{y}}$  is the ambient electric field in the rest frame of the neutral atmosphere. Equations (1) - (3) are two dimensional ( $x, y$ ) where  $x$  is parallel to the relative neutral wind and  $y$  is the direction of  $\underline{E}_o$ . Except for the assumption of constant  $K$ , these equations are accurate to first order in the ratio of ion collision frequency to gyrofrequency. Equation (1) results from multiplying the ion continuity equation by the Pedersen mobility and integrating along the magnetic field. One assumes that the electrostatic potential and therefore  $\underline{V}$  are constant on field lines. The diffusion term in (1) results from the assumption of a constant Pedersen mobility and  $K$  value within the cloud. The assumption of constant  $K$  is admittedly simplistic. For a typical barium cloud without turbulence,  $K$  is roughly proportional to the local plasma density [Perkins et al., 1973]. For a turbulent cloud,  $K$  may be scale size dependent [Goldman and Sperling, 1979]. Attempts to model the variation of  $K$  introduce an additional scaling parameter and tend to muddy the results without changing them significantly. Equation (3) is the equation of quasi-neutrality, which states that the field line integrated electric current,  $\underline{J} = \Sigma \underline{E} = \Sigma(\underline{E}_o - \nabla \phi)$ , must be divergence free.

For the sake of completeness, we should mention that a two layer model with one layer for the cloud and another for the background ionosphere has

been in use for several years [Lloyd and Haerendel, 1973]. One notices that simulations performed with the model tend to yield late time configurations in which there is a strong correlation between density distributions in the two layers [Scannapieco et al., 1976; S. T. Zalesak, private communication, 1980]. This may lend support to one level predictions concerning bifurcation of a particular structure, providing that the conductivity is dominated by the Pedersen component at the cloud level. Equations (1) - (3) may be put into dimensionless form as follows [McDonald, et al., 1978]. Let

$$\begin{aligned}
 \underline{x} &= L_o \underline{x}' \\
 dt &= t_o dt' \\
 \Sigma &= \Sigma_o \Sigma' \\
 \underline{v} &= v_o \underline{v}' \\
 \phi &= L_o E_o \phi' \\
 v_o &= c |E_o / B|, \\
 \text{and} \quad t_o &= L_o / v_o.
 \end{aligned} \tag{4}$$

Here  $L_o$  is a measure of the cloud's gradient scale size, and all primed quantities are dimensionless.  $v_o$  is the relative drift speed between the ambient plasma and the neutral atmosphere, and  $\Sigma_o$  is the ambient integrated Pedersen conductivity. In this paper we take

$$L_o = (\int \Sigma^2 dx dy)^{1/2} / (\int (\nabla \Sigma)^2 dx dy)^{1/2} \tag{5}$$

where the region of integration is a rectangular box containing the structure of interest. We have experimented with more sophisticated definitions of  $L_o$  which are insensitive to the size of the box. These yield results within 20% of those given by (5) for the cases presented here. We prefer to retain the straightforward simplicity of (5).

Substituting (4) into (1) - (3) and dropping primes from all variables we have the dimensionless equations

$$\frac{\partial \Sigma}{\partial t} = - \nabla \cdot \Sigma \underline{V} + R^{-1} \nabla^2 \Sigma \quad (6)$$

$$\underline{V} = - \nabla \phi \times \hat{z} \quad (7)$$

$$\nabla \cdot \Sigma \nabla \phi = \hat{z} \cdot \nabla \Sigma, \quad (8)$$

where  $R = V_o L_o / K. \quad (9)$

Note that R is analogous to the Reynolds number for neutral flows, with the kinematic viscosity replaced by the cross-field plasma diffusivity.

Equations (6) - (8) reveal that the evolution of a plasma cloud is completely determined by initial cloud geometry, boundary conditions, and the value of R. Thus the answer to whether or not a given structure will bifurcate depends upon whether R is greater or smaller than some critical R value applicable to that structure. For sufficiently small R, diffusion will be dominant and will smooth out small structures faster than they can be created. For sufficiently large R, diffusion will be negligible, allowing steepening and bifurcation to proceed.

If the critical R for a particular structure is known, we can use (9) to estimate the scale size of the marginally stable state, providing estimates for  $V_o$  and K are available:

$$L_o = K R / V_o \quad (10)$$

The lifetime of the marginal state may also be estimated. The time required for diffusion to degrade the structure is approximately

$$t_D = L_o^2 / K$$

$$= R L_o / V_o \quad (11)$$

One sees that  $t_D$  is  $R$  times the one dimensional gradient drift instability growth time. Anticipating that  $R$  is a large number, (11) implies that the marginal state can persist for times much greater than basic gradient drift structuring times.

In this work we investigate bifurcations which originate near the tips of striations. This seems to be the most likely place for new structure to emerge, although there is photographic evidence, for example in SPRUCE, that some new structure can emerge from sides of striations. The procedure for estimating the critical  $R$  for a given initial condition on  $\Sigma$  will be to carry out a set of simulations from equations (1) - (3) with assorted values of  $K$ . An upper limit on the critical  $R$  will be taken to be the smallest  $R$  at the time of first bifurcation. A lower limit will be taken as the largest  $R$  among non-bifurcating cases at times used to determine the upper limit. The initial condition on  $\Sigma$  will be taken as an appropriate form representing a single striation tip. This allows numerical resolution to be 4 to 8 times that of our earlier study [McDonald et al., 1978].

### 3. Numerical Simulations

Equations (1) - (3) are advanced in time using numerical techniques described below. A more detailed description of the NRL one-level striations code has been given by McDonald et al., [1979]. We choose the dimensional set rather than (6) - (8) to facilitate comparison with experiment.

With  $\Sigma(x,y)$  given at a particular time, we calculate  $\phi$  from (3), and use the result in (2) to arrive at the flow field  $\underline{V}$ . Then we use (1) to advance  $\Sigma$  by one timestep, after which the cycle can be reinitiated. Finite difference representations are used for all derivatives in (1) - (3).

Solution of the variable coefficient elliptic equation (3) accounts for nearly two-thirds of simulation time for grids as large as that used here (162 by 82 points). We use the Chebychev semi-iterative method to calculate a series of approximations which converge to the true solution of (3) [Varga, 1962; McDonald, 1980]. This method was chosen because of its efficient execution on a vector computer such as the NRL Texas Instruments ASC. It also allows convenient implementation of a wide variety of boundary conditions. Derivatives are represented by second order finite differences on a uniform, non-staggered grid ( $\Sigma$ ,  $\phi$ , and  $\underline{V}$  are calculated on the same set of points). It is possible to obtain an exact solution to the finite difference analog of (3) [Madala, 1978], but computer time and storage requirements become excessive for large grids. We use time extrapolation to obtain an accurate initial approximation to  $\phi$ , and carry out iterations until the root mean square residual error is approximately  $3 \times 10^{-4}$  of the root mean square source term. Reduction of the error much below this level would not necessarily improve results, since discretization introduces errors of this order or greater into the equations.

For the advection term in equation (1) we use the two dimensional flux correction method of Zalesak [1979]. This technique can be incorporated into a number of standard advection schemes to prevent formation of spurious oscillations in the advected quantity. There are two reasons why these oscillations should be avoided: (1) in a divergenceless flow field (see eq. (2)) new maxima or minima cannot be created; and (2) high order schemes can drive  $\Sigma$  negative, resulting in degeneracy of eq. (3) and physically

meaningless velocities. Traditional remedies include local "fill-in" and addition of artificial diffusion globally. The flux correction technique operates locally in regions where the oscillations tend to form, effectively truncating the scheme to first order such that ripples cannot form. The diffusion term in equation (1) is added in a separate step using second order spatial, forward time differencing. In the integration of equation (1) we tacitly subtract from  $\underline{V}$  the structure's centroid velocity. This keeps the interesting structure from drifting off the computational grid. More important, it reduces the number of grid cells through which the structure drifts during a simulation. This helps to reduce discretization error due to the irreversible loss of information that occurs when an arbitrary profile is advected at constant velocity through an Eulerian grid.

The simulations were carried out on a grid of 162 by 82 points in the x and y directions respectively. Each simulation was carried out with a uniform grid interval of 80 meters and was then rerun with a grid interval of 40 meters as a check on the sensitivity of results to resolution. The use of a non-stretched grid increases execution efficiency of the code. The problems arising from electrostatic images on the boundaries are partially alleviated by the use of transmissive boundary conditions described below. The calculation procedure is to update quantities on the interior of the grid (160 x 80 points) by the methods described above, and then calculate exterior values from the boundary conditions.

Boundary conditions used during the simulation are as follows.

Neumann boundaries

$$\frac{\partial}{\partial n} = 0 \quad (12)$$

(with  $n$  the outward normal) are imposed upon  $\Sigma$  and intermediate variables involved in updating equation (1). This allows inflow and outflow of ambient plasma on three sides of the grid where structure does not intersect the boundary (see Figures 1-4). It is also a good approximation for the fourth side (the left boundary of each figure) since  $\Sigma$  contours tend to align with the neutral wind direction ( $x$ ) except near striation tips. For the present study, the Neumann condition seems more realistic than the periodic boundaries used in most earlier simulations. The "re entry" of plasma resulting from periodicity would be nonphysical in the study of an isolated structure.

The physically proper boundary condition on  $\phi$  is that its gradient vanish at infinity. Since we are constrained to a grid of finite extent, we can either stretch the grid to move the boundary far from the structure or attempt to match the interior solution with an appropriate exterior solution. We have chosen an approximation to the second alternative and have developed a physically motivated algorithm which is admittedly simplistic, but has been validated empirically. Our approximate boundary condition is

$$\frac{\partial \phi}{\partial n} + S \frac{\partial^2 \phi}{\partial n^2} = 0 \quad (13)$$

where  $n$  is the outward normal and  $S$  is a constant taken to be the cloud's initial scale size (see (15)). This states that the normal component of the polarization electric field must decrease in the outward direction on a spatial scale comparable to that of the gross structure. We choose to cast (13) in terms of the first two derivatives rather than  $\phi$  and its first derivative so that the addition of a constant to  $\phi$  would have no effect upon structure evolution. We have validated (13) by comparing analytic and finite difference solutions to (3) for elliptic "waterbag" distributions



$\Sigma(x,y)$ . The condition (13) gave results superior to the usual periodic, Neumann, or Dirichlet boundaries.

Initial conditions for the simulations are taken to be descriptive of the tip of a striation (see upper portions of Figures 1-4). Taking the origin at the center of the rectangular grid, we have at  $t = 0$

$$\begin{aligned}\Sigma &= 1 + (M-1) \exp(-y^2/S^2), \quad x < 0 \\ &= 1 + (M-1) \exp(-(x^2+y^2)/S^2), \quad x \geq 0\end{aligned}\tag{14}$$

where  $M$  is the ratio of peak conductivity to ambient. For all cases presented here,

$$S = 1 \text{ km} .\tag{15}$$

The computational domain for results shown in Figures 1-4 is 6.4 by 12.8 kilometers. That we have normalized  $\Sigma$  to the ambient  $\Sigma_0$  has no effect on the model (1) - (3) (i.e.,  $\Sigma$  can be replaced with  $\Sigma/\Sigma_0$ ). All other variables retain their dimensionality. For all cases we take  $B = .5$  gauss, and  $E_0 = -1.67 \times 10^{-7}$  stat volts/cm, so that  $V_0 = 100$  m/s. In this particular simulation it is not necessary to perturb the initial condition, since (14) does not represent a steady state. One must note, however, that discretization and roundoff errors provide effective perturbations to any simulation.

#### 4. Results

Simulation results used to determine upper and lower limits on  $R$  for each of four  $M$  values (2, 5, 10, and 30) are shown in Figures 1-4. For each  $M$ , a set of simulations were carried out for various  $K$  values in order

to help locate the demarcation between bifurcating and non bifurcating states. For each M value we present the two simulations which most accurately bound the critical R. In each case this involves a pair of K values separated by a factor of 2. The range could be narrowed by further simulations, but the approximations involved in taking K constant and specifying boundary conditions at finite distances would lend some uncertainty to the result. Our earlier critical R value for an M = 11 structure [McDonald et al., 1978] is approximately a factor of 2 lower than one would expect from the present work (see Figure 6). We attribute this to the use of different initial conditions, boundary conditions, lower spatial resolution, and a different procedure for determining the critical R.

In each of Figures 1-4 the left column gives contour plots of  $\Sigma$  for cases where K is small enough to permit bifurcation. The plot just below the initial condition plot shows  $\Sigma$  at a time when it is qualitatively clear that bifurcation is about to occur. This time is chosen as appropriate to determine the critical R from (5) and (9). We choose not to determine R at  $t = 0$  because the uniform separation of contours is not "natural." This becomes clear when one examines the non bifurcating states in the right column of Figures 1-4. A quasi stationary state is established only after a sufficient amount of steepening has occurred. It is the stability of a pre-steepened and thus more "natural" state that we wish to address. When the structure is near bifurcation, the selection of a time for calculating R is not crucial. As shown in Figure 5, the length scale tends to level off just prior to the development of new structure. Thus our results are not sensitive to the precise definition of an onset time.

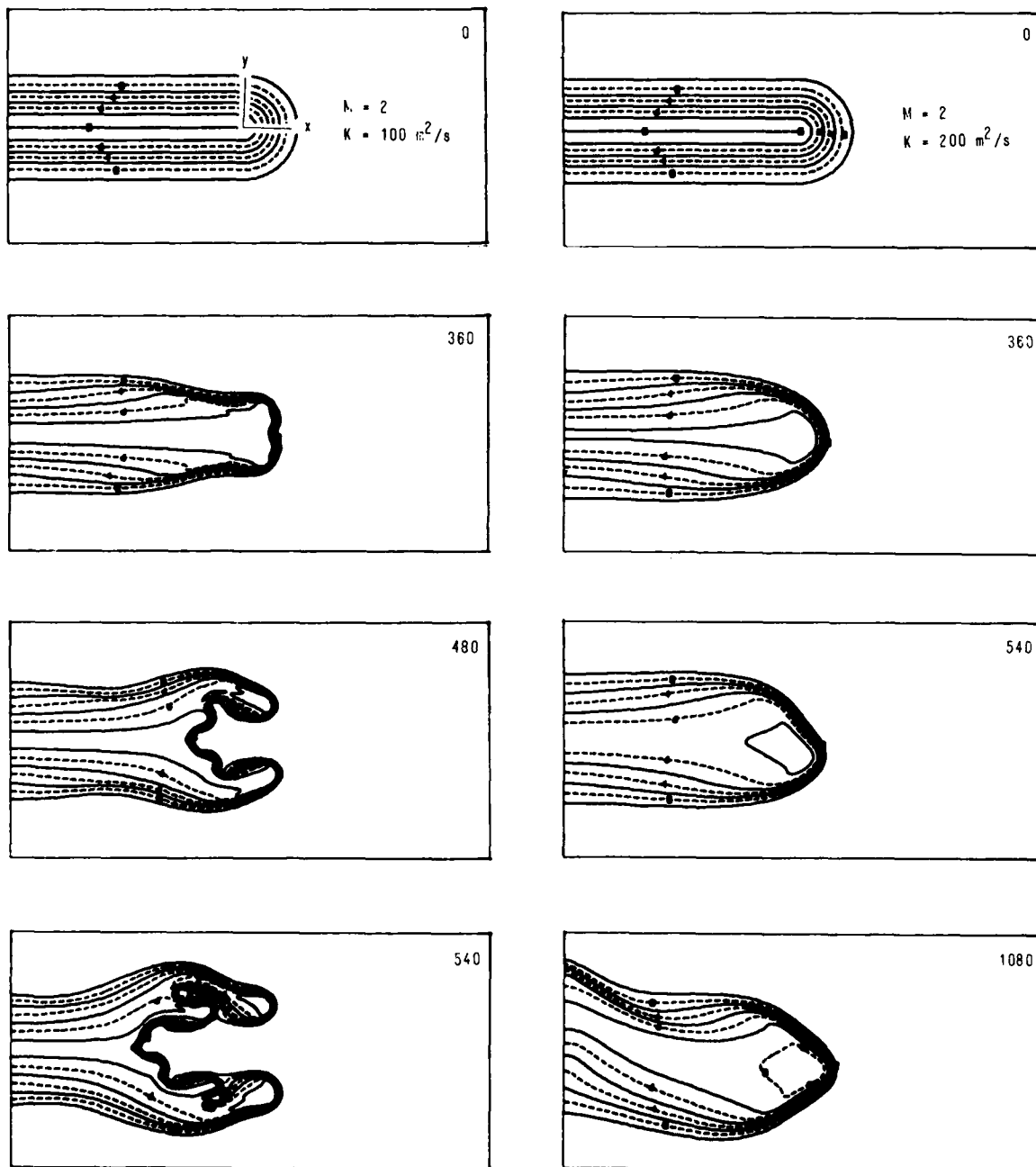


Fig. 1 — Contour plots of  $\Sigma(x,y)$  at selected times illustrating the demarcation between bifurcating (left column) and non-bifurcating (right column) states for  $M = 2$ . Contours are spaced linearly between  $\Sigma = 1$  (ambient) and  $M$ . Limits on the critical  $R$  are evaluated at times when bifurcation of the low  $K$  striation (second plot in left column for Figures 1–4) is eminent. Times appear in the upper right of each plot.

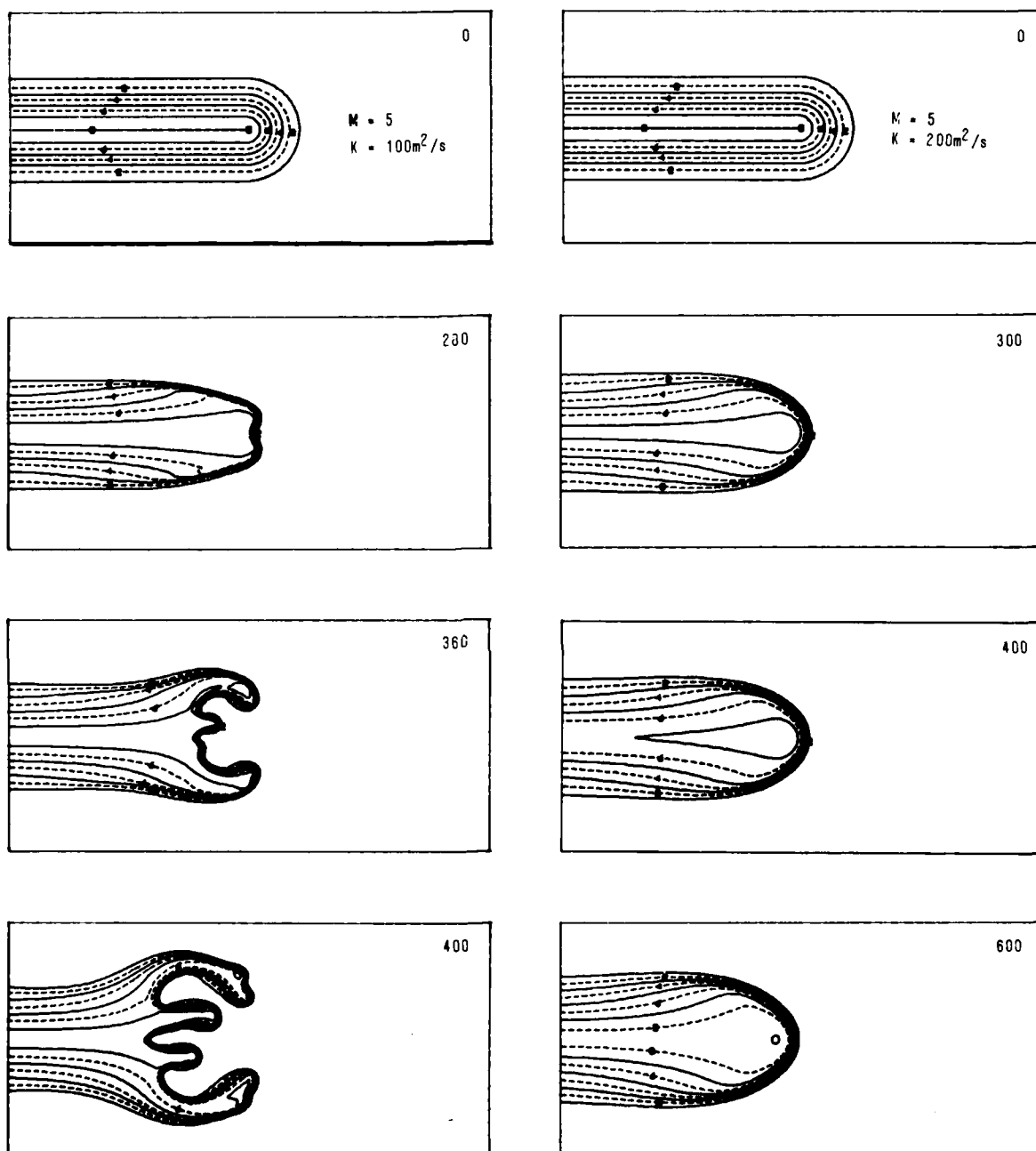


Fig. 2 — Contour plots of  $\Sigma(x,y)$  at selected times illustrating the demarcation between bifurcating (left column) and non-bifurcating (right column) states for  $M = 5$ . The diffusion dominated case is plotted at 300 seconds, the time at which  $L_0$  attains a shallow minimum (see Figure 5). Past this time diffusive dominance is evidenced by the drying up of inner contours.

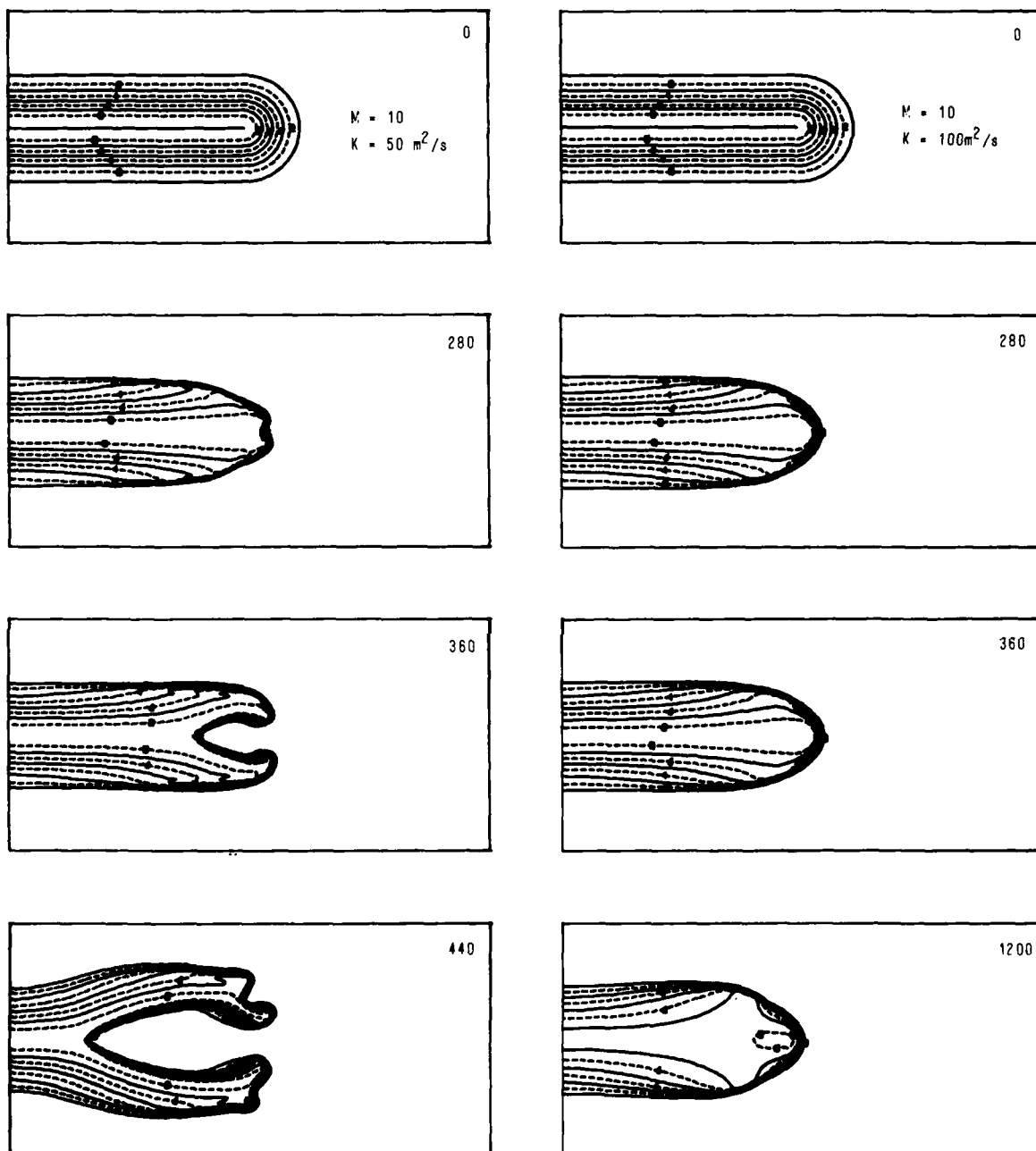


Fig. 3 — Contour plots of  $\Sigma(x,y)$  at selected times illustrating the demarcation between bifurcating (left column) and non-bifurcating (right column) states for  $M = 10$ . Contours are spaced linearly between  $\Sigma = 1$  (ambient) and  $M$ . Limits on the critical  $R$  are evaluated at times when bifurcation of the low  $K$  striation (second plot in left column for Figures 1—4) is eminent. Times appear in the upper right of each plot.

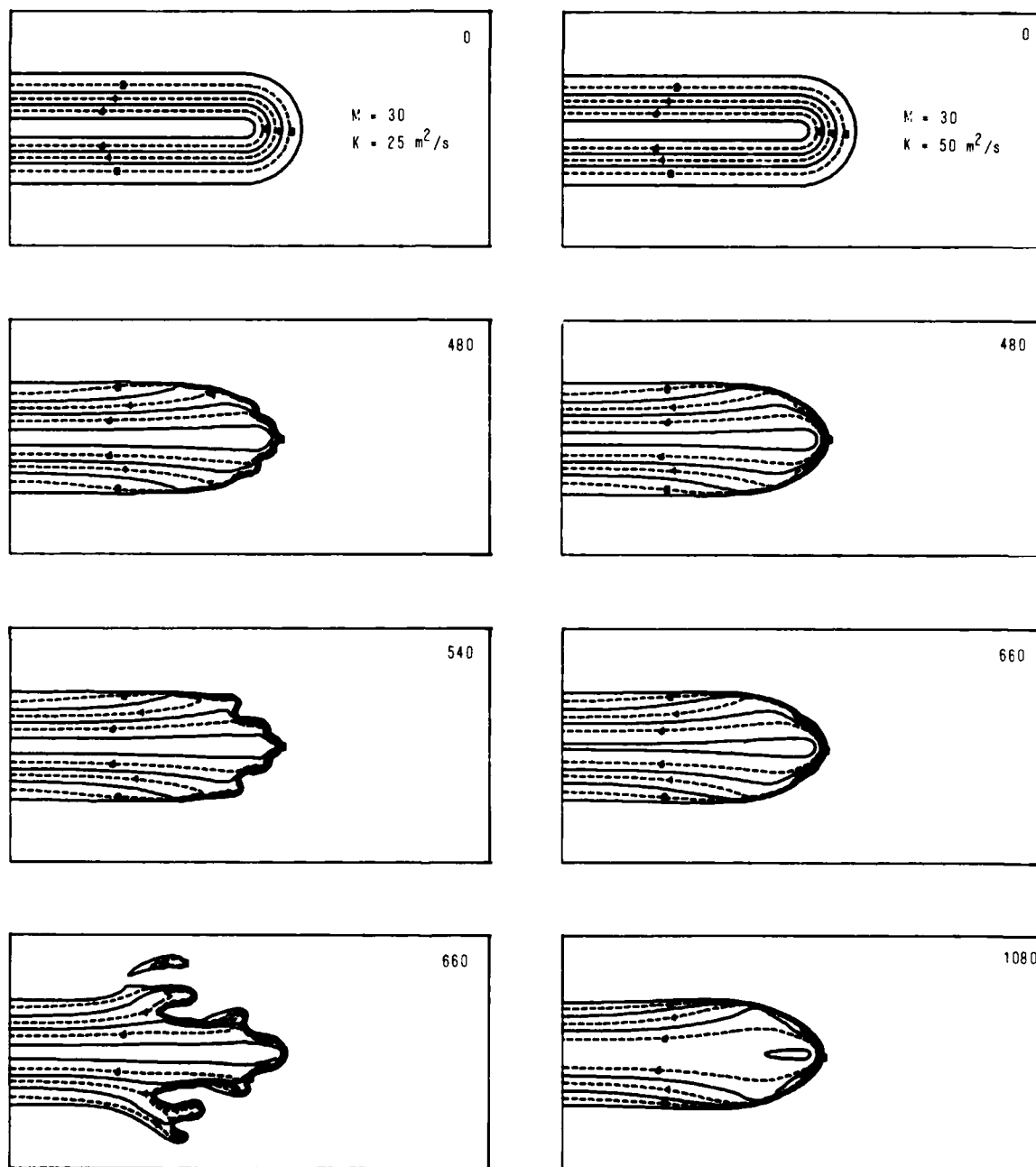


Fig. 4 — Contour plots of  $\Sigma(x,y)$  at selected times illustrating the demarcation between bifurcating (left column) and non-bifurcating (right column) states for  $M = 30$ . Contours are spaced linearly between  $\Sigma = 1$  (ambient) and  $M$ . Limits on the critical  $R$  are evaluated at times when bifurcation of the low  $K$  striation (second plot in left column for Figures 1–4) is eminent. Times appear in the upper right of each plot.

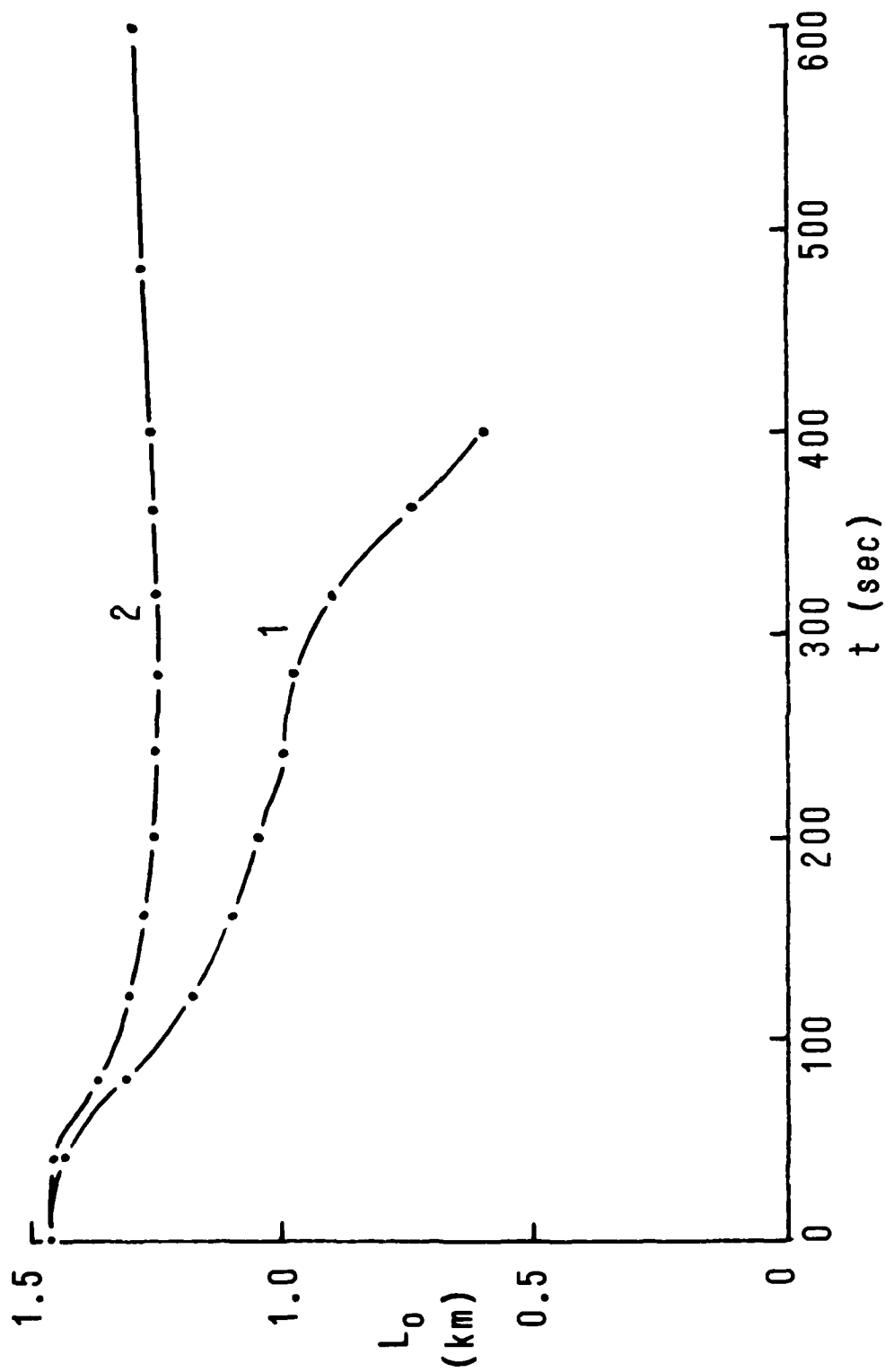


Fig. 5 —  $L_0$  vs time for Figure 2. Curve 1 is the bifurcating case, and curve 2 is the non-bifurcating case

Curves 1 and 2 of Figure 5 shows  $L_0$  as a function of time for the  $M = 5$  simulations. Both curves show an initial transient for  $0 \leq t \leq 125$  sec, indicating that the initial condition is far from a "natural" quasistationary state. For  $125 \leq t \leq 300$  sec, curve 1 shows  $L_0$  slowly decreasing, corresponding to the well known backside steepening phenomenon. Then for  $t > 300$  sec,  $L_0$  decreases rapidly, indicating the onset of bifurcation. This abrupt change in the slope of  $L_0(t)$  coincides with bifurcation in all our runs. In contrast, curve 2 of Figure 5 shows  $L_0$  settling down to a nearly constant value after the transient period.  $L_0$  reaches a shallow minimum at 300 sec., indicating the onset of diffusive dominance rather than bifurcation. The coincidence of this minimum with the knee in curve 1 is fortuitous, since the minimum can be made to occur earlier by increasing the diffusivity.

The bounds on critical  $R$  values gleaned from the simulations are given in Table 1. The column denoted "resolution" refers to results from Figures 1-4 and a duplicate set of simulations performed with twice the spatial resolution on the  $162 \times 82$  grid (boundaries are placed closer to the structure). The degree to which upper and lower bounds are different for different spatial resolution gives a measure of discretization and boundary effects. The geometric means of all  $R$  values from Table 1 are 1207 and 1355 for high and low resolution, respectively, and differ by only 11%. The geometric mean of upper and lower bounds for a given  $M$  is plotted as a function of  $M$  in Figure 6. This plot suggests that the critical  $R$  attains a minimum value between 600 and 700 for  $M \approx 4$ .



Table 1 — Critical R vs. Conductivity Ratio

| M  | Resolution  | Range        |                     | Geometric Mean |
|----|-------------|--------------|---------------------|----------------|
| 2  | High<br>Low | 1629<br>2402 | > R . > 993<br>1527 | 1561           |
| 5  | H<br>L      | 769<br>971   | 450<br>623          | 676            |
| 10 | H<br>L      | 1110<br>1450 | 692<br>853          | 987            |
| 30 | H<br>L      | 4440<br>2722 | 2310<br>1519        | 2552           |

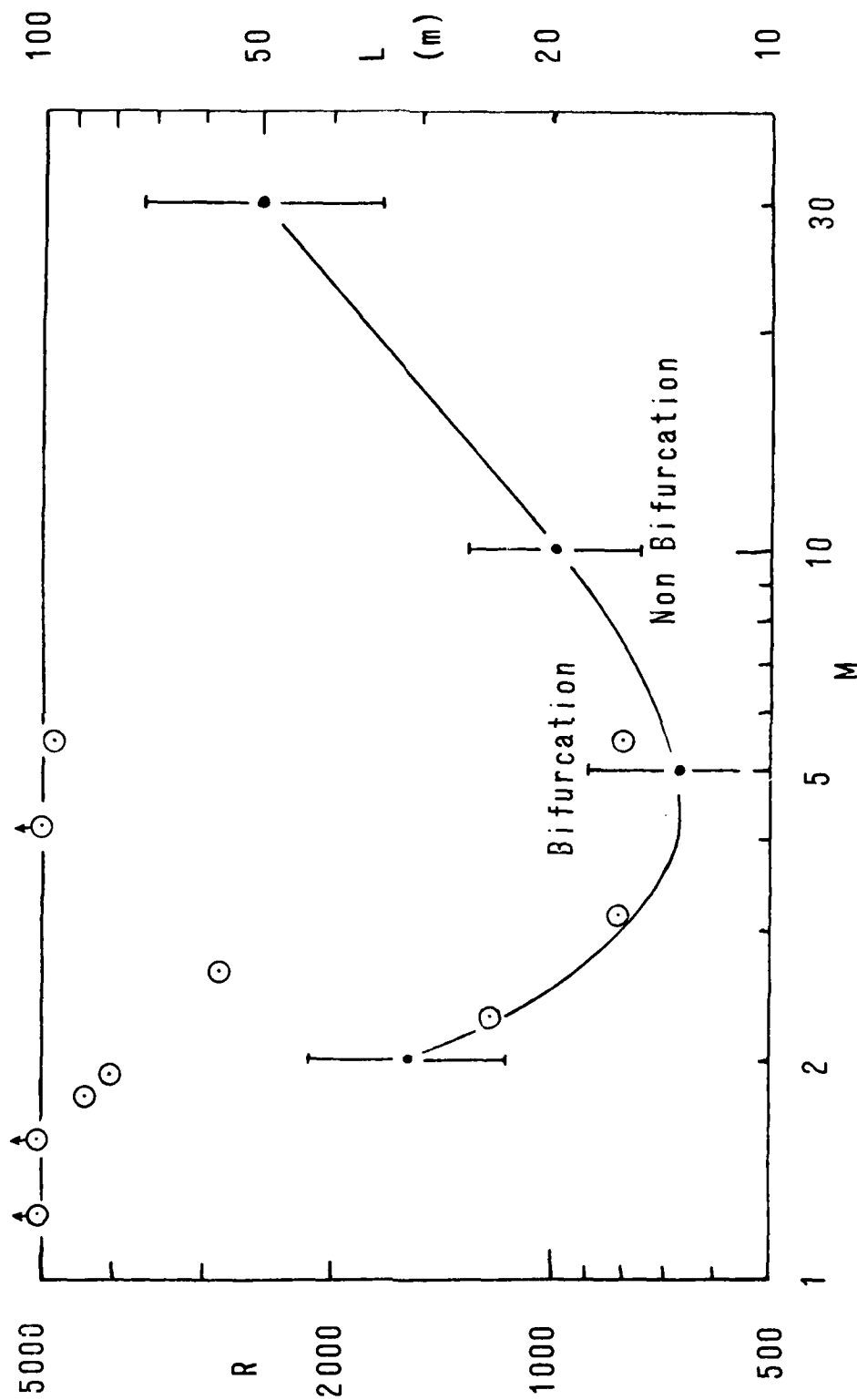


Fig. 6 -- Critical  $R$  vs  $M$ . Solid points: mean values from Table 1. Error bars denote log variances. Circled points: density falloff scale size  $L$  vs  $M$  from rocket data for event Esther [Table 5.1 of Baker et al., 1978].

The shape of this curve is a gratifying result which lends support to the simulations. Linson [1975] offered an ad hoc model to explain observed onset times as a function of  $M$ . This model, based on slip velocities for elliptical piecewise constant density ("waterbag") clouds, predicted a U-shaped curve with a minimum onset time for some  $M > 2$ , the exact value depending on the shape of the cloud. This model was found qualitatively consistent with simulation results for realistic cloud profiles [McDonald et al., 1980]. This minimum onset time may be viewed as a maximum bifurcation tendency. The amount of diffusion required to halt bifurcation is thus maximum at some  $M$  value, resulting in a minimum critical  $R$ . A recent result of Overman and Zabusky [1980] for circular waterbag clouds also supports the qualitative dependence of the critical  $R$  upon  $M$  as shown in Figure 6. They find that shielding and dissipation cooperate so as to produce an effective diffusivity which is the actual diffusivity times  $(M+1)^2/(M-1)$ . If we assume that the amount of effective diffusivity required to halt bifurcation is insensitive to  $M$ , the critical  $R$  should be proportional to  $(M+1)^2/(M-1)$ . This expression has a minimum at  $M = 3$ , in approximate agreement with the curve of Figure 6. In fact, with the exception of the  $M = 2$  case, the expression  $R = 75 (M+1)^2/(M-1)$  gives the mean  $R$  values of Table 1 to 3% accuracy. For high  $M$ , the polarization charges responsible for shielding reside in a thin layer in which the cloud's conductivity rises from ambient to a few times the ambient value. The thinness of this layer results in agreement of the cloud's polarization electric field with that of a suitable waterbag cloud.

Other data from the simulations are presented in Table 2. The marginally stable structures in the right columns of Figs. 1-4 have been Fourier analyzed at times at which the critical  $R$  is evaluated. Summing the two dimensional spectral power over the transverse wavenumber yields one dimen-

sional in situ power spectra  $P(k_x) \propto k_x^{-n_x}$  and  $P(k_y) \propto k_y^{-n_y}$  for the x and y directions respectively. The proportionality is valid only in the central portion of the spectrum. Diffusive dominance is evident in the steepness of the y spectra as compared to the x spectra. This suggests the possibility that a rocket moving transverse to the neutral wind through a "frozen" cloud might find a power spectral density ~~steeper~~ by one or two powers of k than a rocket moving parallel to the neutral wind (assuming that turbulent fluctuations can be removed from the data). Finally, the coupling coefficient  $\zeta$  is given which is simply the ratio of striation centroid velocity  $V_c$  to ambient plasma drift speed  $V_o$  in the frame of the neutral atmosphere. In agreement with analytic results from a waterbag model [Linson, 1975],  $\zeta$  is roughly proportional to  $M^{-1}$  as a result of electric field shielding at high M.

Figures 1-4 reveal that the manner in which an unstable structure comes apart is dependent on the conductivity ratio. For  $M \lesssim 10$ , depletions are able to penetrate the initial structure with ease. However, for  $M \gtrsim 10$ , there is a tendency for the secondary structure to be confined to the surface of the original structure. High conductivity clouds are peeled like an onion, while low conductivity clouds are cut like an apple. This effect is even more apparent in our earlier work [McDonald et al., 1980].

Table 2 — Spectral Indices and Centroid Drifts for Marginally Stable States

| M  | TIME | $n_x$ | $n_y$ | $\zeta = (V_c - V_o)/V_o$ |
|----|------|-------|-------|---------------------------|
| 2  | 360  | 2.2   | 5.4   | 0.634                     |
| 5  | 280  | 1.8   | 4.2   | 0.305                     |
| 10 | 280  | 1.8   | 3.1   | 0.160                     |
| 30 | 480  | 2.0   | 3.1   | 0.057                     |

## 5. Summary and Comparison with Data

For plasma structures resembling striation tips, the model (1) - (3) implies that the demarcation between bifurcating and non bifurcating states is determined by the value of  $R$  (analogous to the Reynolds number in hydrodynamics) and the conductivity ratio  $M$ . This demarcation has been estimated by computer simulation and is presented in Figure 6. The critical  $R$  reaches a minimum of roughly 700 for  $M \approx 4$ . Its dependence upon  $M$  is similar to that of the onset time for striation emergence from a two dimensional cloud [Linson, 1975; McDonald et al., 1980]. This similarity is a result of bifurcation tendency being offset by a proportional amount of diffusion.

Our results compare favorably with three distinct types of experimental observations. These are a) minimum scale sizes as determined by rocket probe data; b) the "freezing-up" of visible structure on scales of approximately one kilometer; and c) the lifetime of the "frozen" state. We shall now discuss each of these areas.

### A. Minimum Scale Sizes

If  $M$  is known for a structure, we can find the critical  $R$  from the curve of Figure 6. We can then use (10) to estimate  $L_0$ , providing we have estimates for  $V_0$  and  $K$ . Since  $L_0$  is proportional to  $K$ , one expects the smallest scales to be determined by the classical (non turbulent) diffusivity

$$K = 2 \frac{\nu_e}{\Omega_e} \frac{ckT}{eB}, \quad (16)$$

where  $\nu_e$  is the sum of electron collision frequencies with cloud ions and ambient neutrals,  $\Omega_e$  is the electron gyrofrequency,  $k$  is Boltzmann's constant,  $T$  is the plasma temperature, and  $e$  is the electron charge. The expression (16) is equivalent to that used in eq. (22) of Perkins et al. [1973].

For plasma number densities  $n \gtrsim 3 \times 10^5 \text{ cm}^{-3}$  at altitudes of 150 km or greater,  $\nu_e$  is dominated by ionic collisions. Thus  $K$  varies approximately as  $nT^{-1/2} B^{-2}$ , as a result of the following.

$$\nu_e \approx \nu_{ei} = (34 + 4.18 \log_{10}(T^3/n)) nT^{-3/2}, \quad (17)$$

where  $n$  is in  $\text{cm}^{-3}$ ,  $T$  is in  $^{\circ}\text{K}$ , and  $\nu_e$  is in  $\text{sec}^{-1}$ . High resolution plasma probe data for the barium cloud Esther [Figure 2 of Baker and Ulwick, 1978] at approximately 170 km give  $5 \times 10^6 \geq n \geq 3 \times 10^5 \text{ cm}^{-3}$ . We have from (16) and (17) with  $T = 1000^{\circ}\text{K}$ ,

$$\begin{aligned} K &= 0.182 \text{ m}^2/\text{s}, \quad n = 3 \times 10^5 \text{ cm}^{-3} \\ &= 2.71 \text{ m}^2/\text{s}, \quad n = 5 \times 10^6 \text{ cm}^{-3} \end{aligned} \quad (18)$$

In order to estimate  $M$  for individual striations in the cloud, we need  $\Sigma$  values in the ambient ionosphere and throughout the cloud (denoted by  $\Sigma_a$  and  $\Sigma_c$ , respectively). Taking a magnetic dip angle  $I = 61.5^{\circ}$  for Eglin AFB, Florida, Francis and Perkins [1975] give for the twilight ionosphere

$$\Sigma_a \approx 3.5 \text{ mho} \quad (19)$$

Since the cloud is contained well above 125 km (where  $\nu_i/\Omega_i \approx 1$  for  $B_a^+$ ) we can take

$$\Sigma_c = \frac{ec}{B} \int n_c \nu_i/\Omega_i dh \csc I, \quad (20)$$

where the path of integration is along the magnetic field,  $h$  is altitude, and field line curvature is neglected. Use of altitude rather than distance along the field facilitates comparison with data. Assuming

$$n_c = n_o \exp(-h^2/D^2),$$

$$v_i = v_o \exp(-h/H),$$

(20) gives

$$\Sigma_c = D n_o \frac{ec}{B} \frac{v_o}{\Omega_i} \csc I \pi^{1/2} \exp(D^2/4H^2). \quad (21)$$

Zero subscripts refer to values at the cloud peak along a given field line.

For conditions applicable to 170 km altitude at sunset, the result of

Linson and Baxter [1977] for  $B_a^+$  gives  $v_o/\Omega_i = .0749$  and  $H = 25.0$  km.

Taking  $B = .5G$ , and  $D = 17.31$  km corresponding to Esther's full width at half maximum [Baker and Ulwick, 1978] of 24 km, (21) gives

$$\Sigma_c = n_o \text{ (cm}^{-3}\text{)} \times 9.433 \times 10^{-6} \text{ mho}$$

The measured values  $5 \times 10^6 \geq n \geq 3 \times 10^5 \text{ cm}^{-3}$  give

$$47.2 \geq \Sigma_c \geq 2.83 \text{ mho}. \quad (23)$$

M values for the individual striations in the Esther cloud are taken to be ratios of  $\Sigma = \Sigma_a + \Sigma_c$  for neighboring peaks and valleys as given by Table 5.1 of Baker et al. [1978]. Scale sizes L for density falloff are given in this table and are plotted as circled points in Figure 6. One sees that minimum scale sizes for a given M are in agreement with our simulation results, providing we take

$$K/V_o = 0.02 \text{ meter}. \quad (24)$$

With  $V_o = 100$  m/s, we have  $K = 2 \text{ m}^2/\text{s}$ , in agreement with the range given by (18). The existence of scale sizes well above the curve of Fig. 6 could be a result of oblique cuts through shanks rather than tips of striations. It could also be a result of an enhanced diffusivity (to be discussed below), lack of complete temporal development, or effects not included in the model (as mentioned in Sec.1).

## B. Kilometer Scale Visible Structure

Departing the issue of minimum scale sizes which seem to be controlled by classical diffusion, our results can be used to address the frequent emergence of visible structure with scale sizes of order 1 kilometer. We hypothesize that plasma turbulence may be involved in these structures. This admits the possibility of individual parcels of plasma macroscopically acting as agents of fluid transport, while microscopically being subject to classical particle diffusion. Thus the smallest structures may reflect electron diffusion dominance, while much larger structures may reflect enhanced diffusivity effects. In order to model these large scale structures, we replace the classical particle diffusivity (16) by an enhanced diffusion term descriptive of a turbulent process. Our goal is not to prove that turbulence is operative, but to offer at least one physically plausible explanation for observed scale sizes and lifetimes.

If we take Bohm diffusion [Chen, 1974]

$$K_B = \frac{1}{16} \frac{ckT}{eB} \quad (25)$$

as descriptive of turbulent diffusivity, we find K values much greater than those given by (16) for typical barium releases. With  $T = 1000^\circ\text{K}$  and  $B = .5 \text{ G}$ , (25) gives  $K_B = 108 \text{ m}^2/\text{s}$ . The curve in Figure 6 suggests that  $R \approx 1000$  is accurate to  $\pm 30\%$  for a range of M values from approximately 2 to 15. Thus (9) would predict  $L_0 \approx 1 \text{ km}$  for the gradient scale size for a variety of typical barium releases in which  $V_0 \approx 100 \text{ m/s}$ . This in agreement with observations cited in the Introduction [J. A. Fedder, W. Chestnut, private communication, 1980].



### C. Lifetime of the Kilometer Scale Structure

If the persistent structure is viewed as marginally stable to bifurcation, its lifetime will be determined by diffusion, and should be in approximate agreement with (11). Using  $L_0 = 1\text{km}$  and  $K_R = 100 \text{ m}^2/\text{s}$ , we find a diffusion time scale of  $10^4 \text{ sec.} = 2.7 \text{ hours}$ . Horizontal drift and sun-lighting conditions make visual tracking of a cloud for this length of time very difficult. However, satellite communications experiments have been conducted for timescales on this order during the STRESS program. For the five STRESS releases, propagation through the clouds resulted in signal fading for durations of 1.4 to 3.7 hours after release [Prettie et al. 1977]. The beam frequency of 341 MHz and the approximate 200 km range from cloud to receiving aircraft implies that the fading was sensitive to structure on scales roughly that of the Fresnel size  $(\lambda z)^{1/2} = 420 \text{ meters}$ .

Acknowledgment. This work was supported by the Defense Nuclear Agency.

## References

- Baker, K. D., J. C. Ulwick, M. C. Kelley, L. C. Howlett, G. D. Allred, D. Delorey, and N. Grossbard, Electron Density Structure in Barium Clouds - Measurements and Interpretation, Final Report, Contract No. DNA 001-76-C-0278, Utah State University, Logan, Utah, February, 1978.
- Baker, K. D., and J. C. Ulwick, Measurements of electron density structure in striated barium clouds, Geophys. Res. Lett. 5, 723, 1978.
- Chen, F. F., Introduction to Plasma Physics, Plenum Press, New York, 1974.
- Francis, S. H., and F. W. Perkins, Determination of striation scale sizes for plasma clouds in the ionosphere, J. Geophys. Res. 80, 3111, 1975.
- Goldman, S. R., and J. L. Sperling, Aspects of late time striation behavior and satellite communication effects, Final Report, Contract No. DNA 001-76-C-P00005, JAYCOR, Inc., Del Mar, California, January 1979.
- Linson, L. M., Slab release and onset time of striatons; in Multiple barium release studies, KMR ionospheric monitoring program, Spring, 1975, HAPREX Final Report V.3, Stanford Research Institute, Menlo Park, California, October, 1975.
- Linson, L. M., and D. C. Baxter, Ion cloud modeling, Final Report, Contract No. DNA 001-76-C-0274, Science Applications, Inc., LaJolla, California, November, 1977.
- Linson, L. M., and J. B. Workman, Formation of striations in ionospheric plasma clouds. J. Geophys. Res. 75, 3211, 1970.
- Lloyd, K.H. and G. Haerendel, Numerical modeling of the drift and deformation of ionospheric plasma clouds and of their interaction with other layers of the ionosphere, J. Geophys. Res., 78, 7389, 1973.
- Madala, R. V., An efficient direct solver for separable and nonseparable elliptic equations, Mon. Weather Rev., 106, 1735, 1978.

- McDonald, B. E. The Chebychev method for solving nonself adjoint elliptic equations on a vector computer, J. Comp. Phys. 35, 147, 1980.
- McDonald, B. E., S. L. Ossakow, S. T. Zalesak, and N. J. Zabusky, Determination of minimum scale sizes in plasma cloud striations, Proc. Symp. on Effect of the Ionosphere on Space and Terrestrial Systems, ed. J. M. Goodman, U.S. Government Printing Office, Stock No. 008-051-00069-1, 1978.
- McDonald, B. E., S. L. Ossakow, S. T. Zalesak, and N. J. Zabusky, Simulation of gradient-drift striations on the ASC, Proc. Scientific Computer Information Exchange Meeting, Office of Basic Energy Sciences, Livermore, California, September 1979.
- McDonald, B. E., M. J. Keskinen, S. L. Ossakow, and S. T. Zalesak, Computer simulation of gradient drift instability processes in operation Avefria, J. Geophys. Res. 85, 2143, 1980.
- Overman, E.A. II, and N. J. Zabusky, Ionospheric plasma cloud (deformable dielectric) stability and nonlinear evolution via regularized contour dynamics, Department of Mathematics and Statistics, University of Pittsburgh, Technical Report ICMA-80-19, July 1980, Pittsburgh, Pa.
- Perkins, F. W., N. J. Zabusky, and J. H. Doles III, Deformation and striation of plasma clouds in the ionosphere, 1, J. Geophys. Res., 78, 697, 1973.
- Prettie, C., A. Johnson, J. Marshall, T. Grizinski, and R. Swanson, Project STRESS satellite communication test results, Air Force Avionics Laboratory, Wright-Patterson AFB, Ohio, Technical Report 77-158, July, 1977.

Scannapieco, A. J., S. L. Ossakow, D. L. Book, B. E. McDonald, and S. R.

Goldman, Conductivity ratio effects on the drift and deformation of  
F region barium clouds coupled to the E region ionosphere, J. Geophys.  
Res., 79, 2913, 1974.

Scannapieco, A. J., S. L. Ossakow, S. R. Goldman and J. M. Pierre, Plasma  
cloud late time striation spectra, J. Geophys. Res. 81, 6037, 1976.

Varga, R. S. Matrix Iterative Analysis, Prentice Hall, Englewood Cliffs, N.J.,  
1962.

Zabusky, N. J., J. H. Doles III, and F. W. Perkins, Deformation and striation  
of plasma clouds in the ionosphere, 2. Numerical simulation of a non-  
linear two-dimensional model, J. Geophys. Res., 78, 711, 1973.

Zalesak, S. T., Fully Multidimensional flux-corrected transport algorithms  
for fluids, J. Comp. Phys. 31, 335, 1979.

## DISTRIBUTION LIST

### DEPARTMENT OF DEFENSE

ASSISTANT SECRETARY OF DEFENSE  
COMM, CMD, CONT & INTELL  
WASHINGTON, D.C. 20301  
OICY ATTN J. BABCOCK  
OICY ATTN M. EPSTEIN

ASSISTANT TO THE SECRETARY OF DEFENSE  
ATOMIC ENERGY  
WASHINGTON, D.C. 20301  
OICY ATTN EXECUTIVE ASSISTANT

DIRECTOR  
COMMAND CONTROL TECHNICAL CENTER  
PENTAGON RM BE 685  
WASHINGTON, D.C. 20301  
OICY ATTN C-650  
OICY ATTN C-312 R. MASON

DIRECTOR  
DEFENSE ADVANCED RSCH PROJ AGENCY  
ARCHITECT BUILDING  
1400 WILSON BLVD.  
ARLINGTON, VA. 22209  
OICY ATTN NUCLEAR MONITORING RESEARCH  
OICY ATTN STRATEGIC TECH OFFICE

DEFENSE COMMUNICATION ENGINEER CENTER  
1860 WIEHLE AVENUE  
RESTON, VA. 22090  
OICY ATTN CODE R820  
OICY ATTN CODE R410 JAMES W. MCLEAN  
OICY ATTN CODE R720 J. WORTHINGTON

DIRECTOR  
DEFENSE COMMUNICATIONS AGENCY  
WASHINGTON, D.C. 20305  
(ADR CNMID: ATTN CODE 240 FOR)  
OICY ATTN CODE 101B

DEFENSE TECHNICAL INFORMATION CENTER  
CAMERON STATION  
ALEXANDRIA, VA. 22314  
(12 COPIES IF OPEN PUBLICATION, OTHERWISE 2 COPIES)  
12CY ATTN TC

DIRECTOR  
DEFENSE INTELLIGENCE AGENCY  
WASHINGTON, D.C. 20301  
OICY ATTN DT-1B  
OICY ATTN DB-4C E. O'FARRELL  
OICY ATTN DIAAP A. WISE  
OICY ATTN DIAST-5  
OICY ATTN DT-1B2 R. MORTON  
OICY ATTN HQ-TR J. STEWART  
OICY ATTN W. WITTIG DC-7D

DIRECTOR  
DEFENSE NUCLEAR AGENCY  
WASHINGTON, D.C. 20305  
OICY ATTN STVL  
OICY ATTN TITL  
OICY ATTN DOST  
OICY ATTN RAAE

COMMANDER  
FIELD COMMAND  
DEFENSE NUCLEAR AGENCY  
KIRTLAND AFB, NM 87115  
OICY ATTN FCPR

DIRECTOR  
INTERSERVICE NUCLEAR WEAPONS SCHOOL  
KIRTLAND AFB, NM 87115  
OICY ATTN DOCUMENT CONTROL

JOINT CHIEFS OF STAFF  
WASHINGTON, D.C. 20301  
OICY ATTN J-3 WMMCCS EVALUATION OFFICE

DIRECTOR  
JOINT STRAT TGT PLANNING STAFF  
OFFUTT AFB  
OMAHA, NB 68113  
OICY ATTN JLTW-2  
OICY ATTN JPST G. GOETZ

CHIEF  
LIVERMORE DIVISION FLD COMMAND DNA  
DEPARTMENT OF DEFENSE  
LAWRENCE LIVERMORE LABORATORY  
P. O. BOX 808  
LIVERMORE, CA 94550  
OICY ATTN FCPL

DIRECTOR  
NATIONAL SECURITY AGENCY  
DEPARTMENT OF DEFENSE  
FT. GEORGE G. MEADE, MD 20755  
OICY ATTN JOHN SKILLMAN R52  
OICY ATTN FRANK LEONARD  
OICY ATTN W14 PAT CLARK  
OICY ATTN OLIVER H. BARTLETT W32  
OICY ATTN R5

COMMANDANT  
NATO SCHOOL (SHAPE)  
APO NEW YORK 09172  
OICY ATTN U.S. DOCUMENTS OFFICER

UNDER SECY OF DEF FOR RSCH & ENGRG  
DEPARTMENT OF DEFENSE  
WASHINGTON, D.C. 20301  
OICY ATTN STRATEGIC & SPACE SYSTEMS (OS)

WMMCCS SYSTEM ENGINEERING ORG  
WASHINGTON, D.C. 20305  
OICY ATTN R. CRAWFORD

COMMANDER/DIRECTOR  
ATMOSPHERIC SCIENCES LABORATORY  
U.S. ARMY ELECTRONICS COMMAND  
WHITE SANDS MISSILE RANGE, NM 88002  
OICY ATTN DELAS-EO F. NILES

DIRECTOR  
BMD ADVANCED TECH CTR  
HUNTSVILLE OFFICE  
P. O. BOX 1500  
HUNTSVILLE, AL 35807  
OICY ATTN ATC-T MELVIN T. CAPPS  
OICY ATTN ATC-O W. DAVIES  
OICY ATTN ATC-R DON RUSS

PROGRAM MANAGER  
BMD PROGRAM OFFICE  
5001 EISENHOWER AVENUE  
ALEXANDRIA, VA 22333  
OICY ATTN DACS-BMT J. SHEA

CHIEF C-E SERVICES DIVISION  
U.S. ARMY COMMUNICATIONS CMD  
PENTAGON RM 1B269  
WASHINGTON, D.C. 20310  
OICY ATTN C-F-SERVICES DIVISION

COMMANDER  
FRADCOM TECHNICAL SUPPORT ACTIVITY  
DEPARTMENT OF THE ARMY  
FORT MONMOUTH, N.J. 07703  
OICY ATTN DRSEL-AL-RD H. BENNET  
OICY ATTN DRSEL-PL-ENV H. BOMKE  
OICY ATTN J. E. QUIGLEY

COMMANDER  
HARRY DIAMOND LABORATORIES  
DEPARTMENT OF THE ARMY  
2800 POWDER MILL ROAD  
ADELPHI, MD 20783  
(CNWDI-INNER ENVELOPE: ATTN: DELHD-RBH)  
O1CY ATTN DELHD-TI M. WEINER  
O1CY ATTN DELHD-RB R. WILLIAMS  
O1CY ATTN DELHD-NP F. WIMENITZ  
O1CY ATTN DELHD-NP C. MOAZED

COMMANDER  
U.S. ARMY COMM-ELEC ENGRG INSTAL AGY  
FT. HUACHUCA, AZ 85613

O1CY ATTN CCC-EMEO GEORGE LANE

COMMANDER  
U.S. ARMY FOREIGN SCIENCE & TECH CTR  
220 7TH STREET, NE  
CHARLOTTESVILLE, VA 22901  
O1CY ATTN DRXST-SD  
O1CY ATTN R. JONES

COMMANDER  
U.S. ARMY MATERIEL DEV & READINESS CMD  
5001 EISENHOWER AVENUE  
ALEXANDRIA, VA 22333  
O1CY ATTN DRCLDC J. A. BENDER

COMMANDER  
U.S. ARMY NUCLEAR AND CHEMICAL AGENCY  
7500 BACKLICK ROAD  
BLDG 2073  
SPRINGFIELD, VA 22150  
O1CY ATTN LIBRARY

DIRECTOR  
U.S. ARMY BALLISTIC RESEARCH LABS  
ABERDEEN PROVING GROUND, MD 21005  
O1CY ATTN TECH LIB EDWARD BAICY

COMMANDER  
U.S. ARMY SATCOM AGENCY  
FT. MONMOUTH, NJ 07703  
O1CY ATTN DOCUMENT CONTINUL

COMMANDER  
U.S. ARMY MISSILE INTELLIGENCE AGENCY  
REDSTONE ARSENAL, AL 35809  
O1CY ATTN JIM GAMBLE

DIRECTOR  
U.S. ARMY TRADOC SYSTEMS ANALYSIS ACTIVITY  
WHITE SANDS MISSILE RANGE, NM 88002  
O1CY ATTN ATAA-SA  
O1CY ATTN TCC/F. PAYAN JR.  
O1CY ATTN ATAA-TAC LTC J. HESSE

COMMANDER  
NAVAL ELECTRONIC SYSTEMS COMMAND  
WASHINGTON, D.C. 20360  
O1CY ATTN NAVALLEX 034 T. HUGHES  
O1CY ATTN PME 117  
O1CY ATTN PME 117-T  
O1CY ATTN CODE 5011

COMMANDING OFFICER  
NAVAL INTELLIGENCE SUPPORT CTR  
4501 SUITLAND ROAD, BLDG. 5  
WASHINGTON, D.C. 20390  
O1CY ATTN MR. DUBBIN STIC 12  
O1CY ATTN NISC-50  
O1CY ATTN CODE 5404 J. GALET

COMMANDER  
NAVAL OCEAN SYSTEMS CENTER  
SAN DIEGO, CA 92152  
O1CY ATTN CODE 532 W. MOLER  
O1CY ATTN CODE 0230 C. BAGGETT  
O1CY ATTN CODE 81 R. EASTMAN

DIRECTOR  
NAVAL RESEARCH LABORATORY  
WASHINGTON, D.C. 20375  
O1CY ATTN CODE 4700 T. P. COFFE (25 CYS IF UN, 1 CY IF CLASS)  
O1CY ATTN CODE 4701 JACK D. BROWN  
O1CY ATTN CODE 4780 BRANCH HEAD (150 CYS IF UN, 1 CY IF CLASS)  
O1CY ATTN CODE 7500 HQ COMM DIR BRUCE WALD  
O1CY ATTN CODE 7550 J. DAVIS  
O1CY ATTN CODE 7580  
O1CY ATTN CODE 7551  
O1CY ATTN CODE 7555  
O1CY ATTN CODE 4730 E. MCLEAN  
O1CY ATTN CODE 4127 C. JOHNSON

COMMANDER  
NAVAL SEA SYSTEMS COMMAND  
WASHINGTON, D.C. 20362  
O1CY ATTN CAPT R. PITKIN

COMMANDER  
NAVAL SPACE SURVEILLANCE SYSTEM  
DAHLGREN, VA 22448  
O1CY ATTN CAPT J. H. BURTON

OFFICER-IN-CHARGE  
NAVAL SURFACE WEAPONS CENTER  
WHITE OAK, SILVER SPRING, MD 20910  
O1CY ATTN CODE F31

DIRECTOR  
STRATEGIC SYSTEMS PROJECT OFFICE  
DEPARTMENT OF THE NAVY  
WASHINGTON, D.C. 20376  
O1CY ATTN NSP-2141  
O1CY ATTN NSSP-2722 FRED WIMBERLY

NAVAL SPACE SYSTEM ACTIVITY  
P. O. BOX 92960  
WORLDWAY POSTAL CENTER  
LOS ANGELES, CALIF. 90009  
O1CY ATTN A. B. HAZZARD

COMMANDER  
NAVAL SURFACE WEAPONS CENTER  
DAHLGREN LABORATORY  
DAHLGREN, VA 22448  
O1CY ATTN CODE DF-14 R. BUTLER

COMMANDING OFFICER  
NAVY SPACE SYSTEMS ACTIVITY  
P.O. BOX 92960  
WORLDWAY POSTAL CENTER  
LOS ANGELES, CA. 90009  
O1CY ATTN CODE 52

OFFICE OF NAVAL RESEARCH  
ARLINGTON, VA 22217  
O1CY ATTN CODE 465  
O1CY ATTN CODE 461  
O1CY ATTN CODE 402  
O1CY ATTN CODE 420  
O1CY ATTN CODE 421

COMMANDER  
AEROSPACE DEFENSE COMMAND/DC  
DEPARTMENT OF THE AIR FORCE  
ENT AFB, CO 80912  
O1CY ATTN DC MR. LONG

COMMANDER  
AEROSPACE DEFENSE COMMAND/XPD  
DEPARTMENT OF THE AIR FORCE  
ENT AFB, CO 80912  
O1CY ATTN XPDQOQ  
O1CY ATTN XP

AIR FORCE GEOPHYSICS LABORATORY  
HANSCOM AFB, MA 01731  
O1CY ATTN OPR HAROLD GARDNER  
O1CY ATTN OPR-1 JAMES C. ULWICK  
O1CY ATTN LKB KENNETH S. W. CHAMPION  
O1CY ATTN OPR ALVA T. STAIR  
O1CY ATTN PHP JULES AARONS  
O1CY ATTN PHD JURGEN BUCHAU  
O1CY ATTN PHD JOHN P. MULLEN

AF WEAPONS LABORATORY  
KIRTLAND AFB, NM 87117

01CY ATTN SUL  
01CY ATTN CA ARTHUR H. GUENTHER  
01CY ATTN OYC CAPT J. BARRY  
01CY ATTN OYC JOHN M. KAMM  
01CY ATTN OYT CAPT MARK A. FRY  
01CY ATTN DES MAJ GARY GANONG  
01CY ATTN OYC J. JANNI

AFTAC  
PATRICK AFB, FL 32925  
01CY ATTN TF/MAJ WILEY  
01CY ATTN TN

AIR FORCE AVIONICS LABORATORY  
WRIGHT-PATTERSON AFB, OH 45433  
01CY ATTN AAD WADE HUNT  
01CY ATTN AAD ALLEN JOHNSON

DEPUTY CHIEF OF STAFF  
RESEARCH, DEVELOPMENT, & ACQ  
DEPARTMENT OF THE AIR FORCE  
WASHINGTON, D.C. 20330  
01CY ATTN AFRDQ

HEADQUARTERS  
ELECTRONIC SYSTEMS DIVISION/XR  
DEPARTMENT OF THE AIR FORCE  
HANSCOM AFB, MA 01731  
01CY ATTN XR J. DEAS

HEADQUARTERS  
ELECTRONIC SYSTEMS DIVISION/YSEA  
DEPARTMENT OF THE AIR FORCE  
HANSCOM AFB, MA 01731  
01CY ATTN YSEA

HEADQUARTERS  
ELECTRONIC SYSTEMS DIVISION/DC  
DEPARTMENT OF THE AIR FORCE  
HANSCOM AFB, MA 01731  
01CY ATTN DCKC MAJ J.C. CLARK

COMMANDER  
FOREIGN TECHNOLOGY DIVISION, AFSC  
WRIGHT-PATTERSON AFB, OH 45433  
01CY ATTN NICD LIBRARY  
01CY ATTN ETOP S. BALLARD

COMMANDER  
ROME AIR DEVELOPMENT CENTER, AFSC  
GRIFFISS AFB, NY 13441  
01CY ATTN DOC LIBRARY/TSLO  
01CY ATTN OCSE V. COYNE

SAMSO/SZ  
POST OFFICE BOX 92960  
WORLDWAY POSTAL CENTER  
LOS ANGELES, CA 90009  
(SPACE DEFENSE SYSTEMS)  
01CY ATTN SZU

STRATEGIC AIR COMMAND/XPFS  
OFFUTT AFB, NE 68113  
01CY ATTN XPFS MAJ B. STEPHAN  
01CY ATTN ADWATE MAJ BRUCE BAUER  
01CY ATTN NRT  
01CY ATTN DOK CHIEF SCIENTIST

SAMSO/SK  
P. O. BOX 92960  
WORLDWAY POSTAL CENTER  
LOS ANGELES, CA 90009  
01CY ATTN SKA (SPACE COMM SYSTEMS) M. CLAVIN

SAMSO/MN  
NORTON AFB, CA 92409  
(MINUTEMAN)  
01CY ATTN MNML LTC KENNEDY

COMMANDER  
ROME AIR DEVELOPMENT CENTER, AFSC  
HANSCOM AFB, MA 01731  
01CY ATTN EEP A. LORENTZEN

DEPARTMENT OF ENERGY  
ALBUQUERQUE OPERATIONS OFFICE  
P. O. BOX 5400  
ALBUQUERQUE, NM 87115  
01CY ATTN DOC CON FOR D. SHERWOOD

DEPARTMENT OF ENERGY  
LIBRARY ROOM G-042  
WASHINGTON, D.C. 20545  
01CY ATTN DOC CON FOR A. LABOWITZ

EG&G, INC.  
LOS ALAMOS DIVISION  
P. O. BOX 809  
LOS ALAMOS, NM 85544  
01CY ATTN DOC CON FOR J. BREEDLOVE

UNIVERSITY OF CALIFORNIA  
LAWRENCE LIVERMORE LABORATORY  
P. O. BOX 808  
LIVERMORE, CA 94550  
01CY ATTN DOC CON FOR TECH INFO DEPT  
01CY ATTN DOC CON FOR L-389 R. OTT  
01CY ATTN DOC CON FOR L-31 R. MAGER  
01CY ATTN DOC CON FOR L-46 F. SEWARD

LOS ALAMOS SCIENTIFIC LABORATORY  
P. O. BOX 1663  
LOS ALAMOS, NM 87545  
01CY ATTN DOC CON FOR J. WOLCOTT  
01CY ATTN DOC CON FOR R. F. TASCHER  
01CY ATTN DOC CON FOR E. JONES  
01CY ATTN DOC CON FOR J. MALIK  
01CY ATTN DOC CON FOR R. JEFFRIES  
01CY ATTN DOC CON FOR J. ZINN  
01CY ATTN DOC CON FOR P. KEATON  
01CY ATTN DOC CON FOR J. WESTERVELT

SANDIA LABORATORIES  
P. O. BOX 5800  
ALBUQUERQUE, NM 87115  
01CY ATTN DOC CON FOR J. MARTIN  
01CY ATTN DOC CON FOR W. BROWN  
01CY ATTN DOC CON FOR A. THORNBROUGH  
01CY ATTN DOC CON FOR T. WRIGHT  
01CY ATTN DOC CON FOR D. DAHLGREN  
01CY ATTN DOC CON FOR 3141  
01CY ATTN DOC CON FOR SPACE PROJECT DIV

SANDIA LABORATORIES  
LIVERMORE LABORATORY  
P. O. BOX 969  
LIVERMORE, CA 94550  
01CY ATTN DOC CON FOR B. MURPHEY  
01CY ATTN DOC CON FOR T. COOK

OFFICE OF MILITARY APPLICATION  
DEPARTMENT OF ENERGY  
WASHINGTON, D.C. 20545  
01CY ATTN DOC CON FOR D. GALE

#### OTHER GOVERNMENT

CENTRAL INTELLIGENCE AGENCY  
ATTN RD/SI, RM 5G48, HQ BLDG  
WASHINGTON, D.C. 20505  
01CY ATTN OSI/PSID RM 5F 19

DEPARTMENT OF COMMERCE  
NATIONAL BUREAU OF STANDARDS  
WASHINGTON, D.C. 20234  
(ALL CORRES: ATTN SEC OFFICER FOR)  
01CY ATTN R. MOORE

INSTITUTE FOR TELECOM SCIENCES  
NATIONAL TELECOMMUNICATIONS & INFO ADMIN  
BOULDER, CO 80303

01CY ATTN A. JEAN (UNCLASS ONLY)  
01CY ATTN W. UTLAUT  
01CY ATTN D. CROMBIE  
01CY ATTN L. BERRY

NATIONAL OCEANIC & ATMOSPHERIC ADMIN  
ENVIRONMENTAL RESEARCH LABORATORIES  
DEPARTMENT OF COMMERCE  
BOULDER, CO 80302

01CY ATTN R. GRUBB  
01CY ATTN AERONOMY LAB G. REID

DEPARTMENT OF DEFENSE CONTRACTORS

AEROSPACE CORPORATION  
P. O. BOX 92957

LOS ANGELES, CA 90009  
01CY ATTN I. GARFUNKEL  
01CY ATTN T. SALMI  
01CY ATTN V. JOSEPHSON  
01CY ATTN S. BOWER  
01CY ATTN N. STOCKWELL  
01CY ATTN D. OLSEN  
01CY ATTN J. CARTER  
01CY ATTN F. MORSE  
01CY ATTN SMFA FOR PMW

ANALYTICAL SYSTEMS ENGINEERING CORP  
5 OLD CONCORD ROAD  
BURLINGTON, MA 01803  
01CY ATTN RADIO SCIENCES

BERKELEY RESEARCH ASSOCIATES, INC.  
P. O. BOX 983  
BERKELEY, CA 94701  
01CY ATTN J. WORKMAN

BOEING COMPANY, THE  
P. O. BOX 3707  
SEATTLE, WA 98124  
01CY ATTN G. KEISTER  
01CY ATTN D. MURRAY  
01CY ATTN G. HALL  
01CY ATTN J. KENNEY

CALIFORNIA AT SAN DIEGO, UNIV OF  
IPAPS, B-019  
LA JOLLA, CA 92093  
01CY ATTN HENRY G. BOOKER

BROWN ENGINEERING COMPANY, INC.  
CUMMINGS RESEARCH PARK  
HUNTSVILLE, AL 35807  
01CY ATTN ROMEO A. DELIBERIS

CHARLES STARK DRAPER LABORATORY, INC.  
555 TECHNOLOGY SQUARE  
CAMBRIDGE, MA 02139  
01CY ATTN D. B. COX  
01CY ATTN J. P. GILMORE

COMPUTER SCIENCES CORPORATION  
6565 ARLINGTON BLVD  
FALLS CHURCH, VA 22046  
01CY ATTN M. BLANK  
01CY ATTN JOHN SPOOR  
01CY ATTN C. NAIL

COMSAT LABORATORIES  
LINTHICUM ROAD  
CLARKSBURG, MD 20734  
01CY ATTN G. HYDE

CORNELL UNIVERSITY  
DEPARTMENT OF ELECTRICAL ENGINEERING  
ITHACA, NY 14850  
01CY ATTN D. T. FARLEY JR

ELECTROSPACE SYSTEMS, INC.  
BOX 1359  
RICHARDSON, TX 75080  
01CY ATTN H. LOGSTON  
01CY ATTN SECURITY (PAUL PHILLIPS)

ESL INC.  
495 JAVA DRIVE  
SUNNYVALE, CA 94086  
01CY ATTN J. ROBERTS  
01CY ATTN JAMES MARSHALL  
01CY ATTN C. W. PRETTIE

FORD AEROSPACE & COMMUNICATIONS CORP  
3939 FABIAN WAY  
PALO ALTO, CA 94303  
01CY ATTN J. T. MATTINGLEY

GENERAL ELECTRIC COMPANY  
SPACE DIVISION  
VALLEY FORGE SPACE CENTER  
GODDARD BLVD KING OF PRUSSIA  
P. O. BOX 8555  
PHILADELPHIA, PA 19101  
01CY ATTN M. H. BORTNER SPACE SCI LAB

GENERAL ELECTRIC COMPANY  
P. O. BOX 1122  
SYRACUSE, NY 13201  
01CY ATTN F. REIBERT

GENERAL ELECTRIC COMPANY  
TEMPO-CENTER FOR ADVANCED STUDIES  
816 STATE STREET (P.O. DRAWER QQ)  
SANTA BARBARA, CA 93102  
01CY ATTN DASIA  
01CY ATTN DON CHANDLER  
01CY ATTN TOM BARRETT  
01CY ATTN TIM STEPHANS  
01CY ATTN WARREN S. KNAPP  
01CY ATTN WILLIAM MCNAMARA  
01CY ATTN B. GAMBILL  
01CY ATTN MACK STANTON

GENERAL ELECTRIC TECH SERVICES CO., INC.  
HMES  
COURT STREET  
SYRACUSE, NY 13201  
01CY ATTN G. MILLMAN

GENERAL RESEARCH CORPORATION  
SANTA BARBARA DIVISION  
P. O. BOX 6770  
SANTA BARBARA, CA 93111  
01CY ATTN JOHN ISE JR  
01CY ATTN JOEL GARBARINO

GEOPHYSICAL INSTITUTE  
UNIVERSITY OF ALASKA  
FAIRBANKS, AK 99701  
(CALL CLASS ATTN: SECURITY OFFICER)  
01CY ATTN T. N. DAVIS (UNCL ONLY)  
01CY ATTN NEAL BROWN (UNCL ONLY)  
01CY ATTN TECHNICAL LIBRARY

GTE SYLVANIA, INC.  
ELECTRONICS SYSTEMS GRP-EASTERN DIV  
77 A STREET  
NEEDHAM, MA 02194  
01CY ATTN MARSHAL CROSS

ILLINOIS, UNIVERSITY OF  
DEPARTMENT OF ELECTRICAL ENGINEERING  
URBANA, IL 61803  
01CY ATTN K. YEH

ILLINOIS, UNIVERSITY OF  
107 COBLE HALL  
801 S. WRIGHT STREET  
URBANA, IL 60680  
(CALL CORRES ATTN SECURITY SUPERVISOR FOR)  
01CY ATTN K. YEH



INSTITUTE FOR DEFENSE ANALYSES  
400 ARMY-NAVY DRIVE  
ARLINGTON, VA 22202

01CY ATTN J. M. AFIN  
01CY ATTN ERNEST BAUER  
01CY ATTN HANS WOLFHARD  
01CY ATTN JOEL BENGSTON

HSS, INC.  
2 ALFRED CIRCLE  
BEDFORD, MA 01730  
01CY ATTN DONALD HANSEN

INT'L TEL & TELEGRAPH CORPORATION  
500 WASHINGTON AVENUE  
NUTLEY, NJ 07110  
01CY ATTN TECHNICAL LIBRARY

JAYCOR  
1401 CAMINO DEL MAR  
DEL MAR, CA 92014  
01CY ATTN S. R. GOLDMAN

JOHNS HOPKINS UNIVERSITY  
APPLIED PHYSICS LABORATORY  
JOHNS HOPKINS ROAD  
LAUREL, MD 20810  
01CY ATTN DOCUMENT LIBRARIAN  
01CY ATTN THOMAS POTEMRA  
01CY ATTN JOHN DASSOULAS

LOCKHEED MISSILES & SPACE CO INC  
P. O. BOX 504  
SUNNYVALE, CA 94088  
01CY ATTN DEPT 60-12  
01CY ATTN D. R. CHURCHILL

LOCKHEED MISSILES AND SPACE CO INC  
3251 HANOVER STREET  
PALO ALTO, CA 94304  
01CY ATTN MARTIN WALT DEPT 52-10  
01CY ATTN RICHARD G. JOHNSON DEPT 52-12  
01CY ATTN W. L. IMHOFF DEPT 52-12

KAMAN SCIENCES CORP  
P. O. BOX 7463  
COLORADO SPRINGS, CO 80933  
01CY ATTN T. MEAGHER

LINKABIT CORP  
10453 ROSELLE  
SAN DIEGO, CA 92121  
01CY ATTN IRWIN JACOBS

M.I.T. LINCOLN LABORATORY  
P. O. BOX 73  
LEXINGTON, MA 02173  
01CY ATTN DAVID M. TOWLE  
01CY ATTN P. WALDRON  
01CY ATTN L. LOUGHLIN  
01CY ATTN D. CLARK

MARTIN MARIETTA CORP  
ORLANDO DIVISION  
P. O. BOX 5837  
ORLANDO, FL 32805  
01CY ATTN R. HEFFNER

MCDONNELL DOUGLAS CORPORATION  
5301 BOLSA AVENUE  
HUNTINGTON BEACH, CA 92647  
01CY ATTN N. HARRIS  
01CY ATTN J. MOULE  
01CY ATTN GEORGE MROZ  
01CY ATTN W. OLSON  
01CY ATTN R. W. MALPRIN  
01CY ATTN TECHNICAL LIBRARY SERVICES

MISSION RESEARCH CORPORATION  
735 STATE STREET  
SANTA BARBARA, CA 93101  
01CY ATTN P. FISCHER  
01CY ATTN W. F. CREVIER  
01CY ATTN STEVEN L. GUTSCHE  
01CY ATTN D. SAPPENFIELD  
01CY ATTN R. BOGUSCH  
01CY ATTN R. HENDRICK  
01CY ATTN RALPH KILB  
01CY ATTN DAVE SOWLE  
01CY ATTN F. FAJEN  
01CY ATTN M. SCHEIBE  
01CY ATTN CONRAD L. LONGMIRE  
01CY ATTN WARREN A. SCHLUETER

MITRE CORPORATION, THE  
P. O. BOX 208  
BEDFORD, MA 01730  
01CY ATTN JOHN MORGANSTERN  
01CY ATTN G. HARDING  
01CY ATTN C. E. CALLAHAN

MITRE CORP  
WESTGATE RESEARCH PARK  
1820 DOLLY MADISON BLVD  
MCLEAN, VA 22101  
01CY ATTN W. HALL  
01CY ATTN W. FOSTER

PACIFIC-SIERRA RESEARCH CORP  
1456 CLOVERFIELD BLVD.  
SANTA MONICA, CA 90404  
01CY ATTN E. C. FIELD JR

PENNSYLVANIA STATE UNIVERSITY  
IONOSPHERE RESEARCH LAB  
318 ELECTRICAL ENGINEERING EAST  
UNIVERSITY PARK, PA 16802  
(NO CLASSIFIED TO THIS ADDRESS)  
01CY ATTN IONOSPHERIC RESEARCH LAB

PHOTOMETRICS, INC.  
442 MARRETT ROAD  
LEXINGTON, MA 02173  
01CY ATTN IRVING L. KOFSKY

PHYSICAL DYNAMICS INC.  
P. O. BOX 3027  
BELLEVUE, WA 98009  
01CY ATTN E. J. FREMOW

PHYSICAL DYNAMICS INC.  
P. O. BOX 10367  
OAKLAND, CA. 94610  
ATTN: A. THOMSON

R & D ASSOCIATES  
P. O. BOX 9695  
MARINA DEL REY, CA 90291  
01CY ATTN FORREST GILMORE  
01CY ATTN BRYAN GABBARD  
01CY ATTN WILLIAM B. WRIGHT JR  
01CY ATTN ROBERT F. LELEVIER  
01CY ATTN WILLIAM J. KARZAS  
01CY ATTN H. ORY  
01CY ATTN C. MACDONALD  
01CY ATTN R. TURCO

RAND CORPORATION, THE  
1700 MAIN STREET  
SANTA MONICA, CA 90406  
01CY ATTN CULLEN CRAIN  
01CY ATTN ED BEDROZIAN

RIVERSIDE RESEARCH INSTITUTE  
80 WEST END AVENUE  
NEW YORK, NY 10023  
01CY ATTN VINCE TRAPANI

SCIENCE APPLICATIONS, INC.

P. O. BOX 2351

LA JOLLA, CA 92038

01CY ATTN LEWIS M. LINSON

01CY ATTN DANIEL A. HAMLIN

01CY ATTN D. SACHS

01CY ATTN E. A. STRAKER

01CY ATTN CURTIS A. SMITH

01CY ATTN JACK MCDUGALL

RAYTHEON CO.

528 BOSTON POST ROAD

SUDBURY, MA 01776

01CY ATTN BARBARA ADAMS

Science Applications, Inc.

1700 Goodridge Dr.

McLean, Va. 22102

01 cy ATTN J. COCKAYNE

Lockheed Missile & Space Co., Inc.

Huntsville Research & Engineering  
Center

4800 Bradford Dr.

Huntsville, Ala. 35807

01 cy ATTN DALE H. DIVIS

SRI INTERNATIONAL

333 RAVENSWOOD AVENUE

MENLO PARK, CA 94025

01CY ATTN DONALD NEILSON

01CY ATTN ALAN BURNS

01CY ATTN G. SMITH

01CY ATTN L. L. COBB

01CY ATTN DAVID A. JOHNSON

01CY ATTN WALTER G. CHESNUT

01CY ATTN CHARLES L. RINO

01CY ATTN WALTER JAYE

01CY ATTN M. BARON

01CY ATTN RAY L. LEADABRAND

01CY ATTN G. CARPENTER

01CY ATTN G. PRICE

01CY ATTN J. PETERSON

01CY ATTN R. HAKE, JR.

01CY ATTN V. GONZALES

01CY ATTN D. MCDANIEL

TECHNOLOGY INTERNATIONAL CORP

75 WIGGINS AVENUE

BEDFORD, MA 01730

01CY ATTN W. P. BOQUIST

TRW DEFENSE & SPACE SYS GROUP

ONE SPACE PARK

REDONDO BEACH, CA 90278

01CY ATTN R. K. PLEBUCH

01CY ATTN S. ALTSCHULER

01CY ATTN D. DEE

VISIODYNE, INC.

19 THIRD AVENUE

NORTH WEST INDUSTRIAL PARK

BURLINGTON, MA 01803

01CY ATTN CHARLES HUMPHREY

01CY ATTN J. W. CARPENTER

IONOSPHERIC MODELING DISTRIBUTION LIST  
UNCLASSIFIED ONLY

PLEASE DISTRIBUTE ONE COPY TO EACH OF THE FOLLOWING PEOPLE:

ADVANCED RESEARCH PROJECTS AGENCY (ARPA)  
STRATEGIC TECHNOLOGY OFFICE  
ARLINGTON, VIRGINIA

CAPT. DONALD M. LEVINE

NAVAL RESEARCH LABORATORY  
WASHINGTON, D.C. 20375

DR. P. MANGE  
DR. R. MEIER  
DR. E. SZUSZCZEWICZ - CODE 4127

DR. J. GOODMAN - CODE 7560

SCIENCE APPLICATIONS, INC.  
1250 PROSPECT PLAZA  
LA JOLLA, CALIFORNIA 92037

DR. D. A. HAMLIN  
DR. L. LINSON  
DR. D. SACHS

DIRECTOR OF SPACE AND ENVIRONMENTAL LABORATORY  
NOAA  
BOULDER, COLORADO 80302

DR. A. GLENN JEAN  
DR. G. W. ADAMS  
DR. D. N. ANDERSON  
DR. K. DAVIES  
DR. R. F. DONNELLY

A. F. GEOPHYSICS LABORATORY  
L. G. HANSOM FIELD  
BEDFORD, MASS. 01730

DR. T. ELKINS  
DR. W. SWIDER  
MRS. R. SAGALYN  
DR. J. M. FORBES  
DR. T. J. KENESHEA  
DR. J. AARONS

OFFICE OF NAVAL RESEARCH  
800 NORTH QUINCY STREET  
ARLINGTON, VIRGINIA 22217

DR. H. MULLANEY

COMMANDER  
NAVAL ELECTRONICS LABORATORY CENTER  
SAN DIEGO, CALIFORNIA 92152

DR. M. BLEIWEISS  
DR. I. ROTHMULLER  
DR. V. HILDEBRAND  
MR. R. ROSE

U. S. ARMY ABERDEEN RESEARCH AND DEVELOPMENT CENTER  
BALLISTIC RESEARCH LABORATORY  
ABERDEEN, MARYLAND

DR. J. HEIMERL

COMMANDER  
NAVAL AIR SYSTEMS COMMAND  
DEPARTMENT OF THE NAVY  
WASHINGTON, D.C. 20360

DR. T. CZUBA

HARVARD UNIVERSITY  
HARVARD SQUARE  
CAMBRIDGE, MASS. 02138

DR. M. B. MCELROY  
DR. R. LINDZEN

PENNSYLVANIA STATE UNIVERSITY  
UNIVERSITY PARK, PENNSYLVANIA 16802

DR. J. S. NISBET  
DR. P. R. ROHRBAUGH  
DR. D. E. BARAN  
DR. L. A. CARPENTER  
DR. M. LEE  
DR. R. DIVANY  
DR. P. BENNETT  
DR. E. KLEVANS

UNIVERSITY OF CALIFORNIA, LOS ANGELES  
405 HILLGARD AVENUE  
LOS ANGELES, CALIFORNIA 90024

DR. F. V. CORONITI  
DR. C. KENNEL

UNIVERSITY OF CALIFORNIA, BERKELEY  
BERKELEY, CALIFORNIA 94720

DR. M. HUDSON

UTAH STATE UNIVERSITY  
4TH N. AND 8TH STREETS  
LOGAN, UTAH 84322

DR. P. M. BANKS  
DR. R. HARRIS  
DR. V. PETERSON  
DR. R. MEGILL  
DR. K. BAKER

CORNELL UNIVERSITY  
ITHACA, NEW YORK 14850

DR. W. E. SWARTZ  
DR. R. SUDAN  
DR. D. FARLEY  
DR. M. KELLEY

NASA  
GODDARD SPACE FLIGHT CENTER  
GREENBELT, MARYLAND 20771

DR. S. CHANDRA  
DR. K. MAEDO

PRINCETON UNIVERSITY  
PLASMA PHYSICS LABORATORY  
PRINCETON, NEW JERSEY 08540

DR. F. PERKINS  
DR. E. FRIEMAN

INSTITUTE FOR DEFENSE ANALYSIS  
400 ARMY/NAVY DRIVE  
ARLINGTON, VIRGINIA 22202

DR. E. BAUER

UNIVERSITY OF MARYLAND  
COLLEGE PARK, MD 20742  
DR. K. PAPADOPOULOS  
DR. E. OTT

UNIVERSITY OF PITTSBURGH  
PITTSBURGH, PA. 15213

DR. N. ZABUSKY  
DR. M. BIONDI

UNIVERSITY OF CALIFORNIA  
LOS ALAMOS SCIENTIFIC LABORATORY  
J-10, MS-664  
LOS ALAMOS, NEW MEXICO 87545

M. PONGRATZ  
D. SIMONS  
G. BARASCH  
L. DUNCAN

**DAT  
FILM**